## Development of intelligent systems (RInS)

## Robot manipulation

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Literature: Tadej Bajd (2006) Osnove robotike, poglavje 4
Anže Rezelj (2017) Razvoj nizkocenovnega lahkega robotskega manipulatorja
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## Robot manipulator

- Industrial robot as defined by the standard ISO 8373:

An automatically controlled, reprogrammable, multipurpose manipulator programmable in three or more axes, which can be either fixed in place or mobile for use in industrial automation applications.


## Characteristics

- Closed-loop control
- Electrical or hydraulic motors
- Sensors
- Proprioceptive: rotation encoders, measurement od distance, speed
- Exteroceptive: tactile sensors, robot vision
- Reprogrammable:
- designed so that the programmed motions or auxiliary functions can be changed without physical alteration
- Multipurpose:
- capable of being adapted to a different application with physical alteration
- Physical alteration:
- alteration of the mechanical system
- fixed or mobile robots
- Axis: direction used to specify the robot motion in a linear or rotary mode
- 3 or more DOF


## Robot manipulator

- Arm+wrist+end effector/gripper
- 6DOF - can put an object in an arbitrary pose
- arm positions the object into the desired position
- wrist rotates it into the desired orientation
- gripper grasps the object



## Robot arm

- Serial chain of three links
- connected by joints
- Revolute/rotational joint

- Prismatic/translational joint



## Robot arm types

- Joints
- Revolute/rotational
- Prismatic/translational
- Axis of two neigbouring links
- Parallel
- Perpendicular
- 3DOF
- In practice typically five different arms:
- Anthropomorphic
- Spherical
- SCARA
- Cylindrical
- Cartesian


## Anthropomorphic robot arm

- Three rotational joints (RRR)
- Workspace: sphere-like
- Resembles a human arm



## Spherical robot arm

- Two rotational, one translational joint (RRT)
- Workspace: sphere-like



## SCARA robot arm

- Selective Articulated Robot for Assembly
- Two rotational, one translational joint (RRT)
- Workspace: cylinder-like



## Cylindrical robot arm

- One rotational, two translational joints (RTT)
- Workspace: cylinder



## Cartesian robot arm

- Three translational joints (TTT)
- Workspace: cuboid



## Robot wrist

- Rotates the object in an arbitrary orientation
- Three rotational joints (RRR)
- Sometimes also one or two suffice
- Links should be as short as possible



## Robot end-effector

- The final link of the robot manipulator
- Grippers with fingers
- With two fingers
- With more than two fingers
- Other type of grippers
- Vacuum
- Magnetic
- Perforation

- Other tools as end-effectors
- Welding gun
- Spray painting gun



## Robot workspace

- Reachable workspace
- The end-effector can reach every point in this space
- Dexterous workspace
- The end-effector can reach every point in tis space from the arbitrary orientation



## Kinematics

- Base coordinate frame $\left[X_{1}, Y_{1}, Z_{1}\right]$
- Usually also world coordinate frame
- Used for defining of the robotic task
- End-effector reference frame [ $X_{m}, Y_{m}, Z_{m}$ ]
- End-effector position
- Vector between the origins of the coordinate frames
- Object orientation
- Three angles
- Internal robot coordinates / joint variables
- Joint states (angles, translations)
- Uniquely describe the pose of the robot

- Direct kinematics
- Determine the external robot coordinates from the internal coordinates
- Inverse kinematics
- Determine the internal robot coordinates from the external coordinates


## Geometrical robot model

- Robot manipulator = a serial chain of segments connected by joints
- Every joint can be either rotational or translational
- 1DOF - 1 internal coordinate

- Geometrical robot model describes
- the pose of the last segment of the robot (end-effector) expressed in the reference (base) frame
- depending on the current internal coordinates


## Geometrical robot model

- Geometrical model can be expressed by a homogenuous transformation:

$$
\mathbf{T}^{0}(\mathbf{q})=\left[\begin{array}{ccc}
\mathfrak{n}^{\circ}(\mathbf{q}) & \mathbf{s}^{\circ}(\mathbf{q}) & \mathfrak{a}^{\circ}(\mathbf{q}) \\
0 & 0 & 0 \\
\mathbf{p}^{o}(\mathbf{q}) \\
1
\end{array}\right]
$$

- p : position of the end effector in the reference coordinate frame
- $\mathbf{n}, \mathbf{s}, \mathbf{a}$ : unit vectors of the end-effector coordinate frame:
- a: approach
- s: sliding
- n: normal
- q : vector of internal coordinates



## Poses of segments

- Every joint connects two neighbouring segments/links
- Determine the transformation between them
- Recursively build the full model for the entire robot
- Coordinate frames can be arbitrarily attached to the individual segments
- Denavit - Hartenberg rules simplify computation of the geometrical robot model
- Determine the pose of the i-th c.f. with respect to the pose of the (i-1)-th c.f.
- Axis i connects segments ( $\mathrm{i}-1$ ) and i



## Denavit - Hartenberg rules

- Describe the coordinate frame of the $i$-th segment (having the joint $i+1$ ):

1. Define the axis $z_{i}$ through the axis of the joint $i+1$
2. Find the common normal, perpendicular to the axes $z_{i-1}$ and $z_{i}$

- Position the origin of $O_{i}$ into the intersection of the axis $z_{i}$ with the common normal
- Position the origin of $\mathrm{O}_{\mathrm{i}}$, into the intersection of the axis $\mathrm{z}_{\mathrm{i}-1}$ with the common normal
- If the axes are parallel, position the origin anywhere

3. Position the axis $x_{i}$ on a common normal in a way, that it is oriented from the joint $i$ towards the joint $\mathrm{i}+1$

- If the axis $z_{i-1}$ and $z_{i}$ intersect, orient the axis $x_{i}$ perpendicular to the plane defined by the axes $\mathrm{z}_{\mathrm{i}-1}$ in $\mathrm{z}_{\mathrm{i}}$

4. Determine the axis $y_{i}$ in a way that gives the rigt-handed c.f.

- Similarly we also describe (have already described) the coordinate frame of the segment (i-1)
- The origin $\mathrm{O}_{\mathrm{i}-1}$ is determined by the intersection of the common normal of the axes $\mathrm{i}-1$ and i
- The axis $z_{i-1}$ is oriented along the $i$-th axis
- $x_{i-1}$ is oriented along the common normal and directed from the joint $i-1$ towards the joint $i$


## Graphical illustration of DH parameters



## Denavit - Hartenberg parameters

- The pose of i -th c.f. with respect to ( $\mathrm{i}-1$ )-th c.f. is determined by 4 parameters:

1. (aid distance between $O_{i}$ and $O_{i}$ along $x_{i}$
2. $d_{i}$ - distance between $\mathrm{O}_{\mathrm{i}-1}$ and $\mathrm{O}_{\mathrm{i}}$, along $\mathrm{z}_{\mathrm{i}-1}$
3. $a_{i}$ - angle between $z_{i-1}$ and $z_{i}$ around $x_{i}$
4. $\theta_{i}$ - angle between $x_{i-1}$ and $x_{i}$ around $z_{i-1}$


## Denavit - Hartenberg parameters



## Denavit - Hartenberg parameters

- $\mathrm{a}_{\mathrm{i}}$ and $\mathrm{a}_{\mathrm{i}}$ are always constant
- They depend on the geometry of the robot, the links between the joints, etc.
- They do not change during the operation of the robot
- One of the two remaining parameters is a variable
- $\Theta_{i}$, if the i-th joint is rotational
- $d_{i}$, if the $i$-th joint is translational


## Denavit - Hartenberg parameters

- Illustration
- $\mathrm{r}=\mathrm{a}$
- $\mathrm{n}=\mathrm{i}$


Wikipedia

## Denavit - Hartenberg parameters

- Video:


## Denavit-Hartenberg Reference Frame Layout

Produced by Ethan Tira-Thompson

http://en.wikipedia.org/wiki/Denavit-Hartenberg_Parameters

## Exceptions

- Some exceptions in certain situations can be used to simplify the process:
- Axis $\mathrm{z}_{\mathrm{i}}$ and $\mathrm{z}_{\mathrm{i}-1}$ are parallel $->\mathrm{d}_{\mathrm{i}}=0$
- Axis $z_{i}$ and $z_{i-1}$ intersect -> $O_{i}$ is in the intersection
- In case of the base ( 0 -th) segment: only the axis $z_{0}$ is defined
$->$ put the origin of $\mathrm{O}_{0}$ in the first joint
$->$ align $x_{0}$ and $x_{1}$
- In case of end-effector (n-th c.f.):

Only axis $x_{n}$ is defined; it is perpendicular to $z_{n-1}$
$->z_{n}$ should be parallel to $z_{n-1}$

- In case of translational joint:
-> orient the axis $z_{i-1}$ in the direction of translation
-> position $\mathrm{O}_{\mathrm{i}-1}$ at the beginning of translation


## Denavit - Hartenberg transformation

- Transformation between the i-th and (i-1)-th c.f.:

1. Take the c.f. $\mathrm{O}_{\mathrm{i}-1}$ attached to the segment ( $\mathrm{i}-1$ )
2. Translate it for $d_{i}$ and rotate it for $\Theta_{i}$ along and around $z_{i-1}$, to align it with the c.f. $\mathrm{O}_{\mathrm{i}}$.
3. Translate c.f. $O_{i}$ for $a_{i}$ in rotate it for $a_{i}$ along and around $\mathrm{x}_{\mathrm{i}}$, , to align it with the c.f. $\mathrm{O}_{\mathrm{i}}$
4. DH transformation is obtained by postmultiplication of both transformation matrices - Function of a single variable:

- $\Theta_{i}$ for rotational joint
- $\mathrm{d}_{\mathrm{i}}$ for translational joint

$$
\mathbf{A}_{i^{\prime}}^{i-1}=\left[\begin{array}{cccc}
c \theta_{i} & -s \theta_{i} & 0 & 0 \\
s \theta_{i} & c \theta_{i} & 0 & 0 \\
0 & 0 & 1 & d_{i} \\
0 & 0 & 0 & 1
\end{array}\right]
$$

$$
\mathbf{A}_{i}^{i-1}\left(q_{i}\right)=\mathbf{A}_{i^{\prime}}^{i-1} \cdot \mathbf{A}_{i}^{i^{\prime}}=\left[\begin{array}{cccc}
c \theta_{i} & -s \theta_{i} c \alpha_{i} & s \theta_{i} s \alpha_{i} & a_{i} c \theta_{i} \\
s \theta_{i} & c \theta_{i} c \alpha_{i} & -c \theta_{i} s \alpha_{i} & a_{i} s \theta_{i} \\
0 & s \alpha_{i} & c \alpha_{i} & d_{i} \\
0 & 0 & 0 & 1
\end{array}\right]
$$

## Calculation of the geometrical robot model

1. Set the coordinate frames for all segments
2. Define the table of DH parameters $a_{i}, d_{i}, \alpha_{i}$ in $\theta_{i}$ for all segments $i=1,2, \ldots, n$
3. Calculate DH transformations $\mathbf{A}_{i}^{i-1}\left(q_{i}\right)$ for $\mathrm{i}=1,2, \ldots, \mathrm{n}$
4. Calculate the geometrical model: $\mathbf{T}_{n}^{o}(\mathbf{q})=\mathbf{A}_{1}^{o}\left(q_{1}\right) \cdot \mathbf{A}_{2}^{1}\left(q_{2}\right) \cdots \mathbf{A}_{n}^{n-1}\left(q_{n}\right)$


## Using geometrical model

- Geometrical robot model gives the pose of the last segment of the robot (endeffector) expressed in the reference (base) frame
- Geometrical robot model defines the pose (position and orientation) of the endeffector depending on the current internal coordinates $\mathbf{q}$



## Anthropomorphic robot manipulator



## Anthropomorphic robot manipulator

| Segment | $\mathrm{a}_{\mathrm{i}}$ | $\alpha_{\mathrm{i}}$ | $\mathrm{d}_{\mathrm{i}}$ | $\theta_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | $\pi / 2$ | 0 | $\theta_{1}$ |
| 2 | $\mathrm{a}_{2}$ | 0 | 0 | $\theta_{2}$ |
| 3 | $\mathrm{a}_{3}$ | 0 | 0 | $\theta_{3}$ |

$$
\mathbf{A}_{i}^{i-1}\left(q_{i}\right)=\left[\begin{array}{cccc}
c \theta_{i} & -s \theta_{i} c \alpha_{i} & s \theta_{i} s \alpha_{i} & a_{i} c \theta_{i} \\
s \theta_{i} & c \theta_{i} c \alpha_{i} & -c \theta_{i} s \alpha_{i} & a_{i} s \theta_{i} \\
0 & s \alpha_{i} & c \alpha_{i} & d_{i} \\
0 & 0 & 0 & 1
\end{array}\right]
$$

$$
\begin{gathered}
\mathbf{A}_{1}^{o}\left(\theta_{1}\right)=\left[\begin{array}{cccc}
c_{1} & 0 & s_{1} & 0 \\
s_{1} & 0 & -c_{1} & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \quad \mathbf{A}_{i}^{i-1}\left(\theta_{1}\right)=\left[\begin{array}{cccc}
c_{i} & -s_{i} & 0 & a_{i} c_{i} \\
s_{i} & c_{i} & 0 & a_{i} s_{i} \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \quad \mathrm{i}=2,3 \\
\mathbf{T}_{3}^{o}(\mathbf{q})=\mathbf{A}_{1}^{o} \cdot \mathbf{A}_{2}^{1} \cdot \mathbf{A}_{3}^{2}=\left[\begin{array}{cccc}
\mathrm{c}_{1} \mathrm{c}_{23} & -\mathrm{c}_{1} \mathrm{~s}_{23} & \mathrm{~s}_{1} & \mathrm{c}_{1}\left(\mathrm{a}_{2} \mathrm{c}_{2}+\mathrm{a}_{3} \mathrm{c}_{23}\right) \\
\mathrm{s}_{1} \mathrm{c}_{23} & -\mathrm{s}_{1} \mathrm{~s}_{23} & -\mathrm{c}_{1} & \mathrm{~s}_{1}\left(\mathrm{a}_{2} \mathrm{c}_{2}+\mathrm{a}_{3} \mathrm{c}_{23}\right) \\
\mathrm{s}_{23} & \mathrm{c}_{23} & 0 & \mathrm{a}_{2} \mathrm{~s}_{2}+\mathrm{a}_{3} \mathrm{~s}_{23} \\
0 & 0 & 0 & 1
\end{array}\right]
\end{gathered}
$$

## Stanford robot manipulator



## Stanford robot manipulator

| Segment | $\mathrm{a}_{\mathrm{i}}$ | $\alpha_{\mathrm{i}}$ | $\mathrm{d}_{\mathrm{i}}$ | $\theta_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | $-\pi / 2$ | 0 | $\theta_{1}$ |
| 2 | 0 | $\pi / 2$ | $\mathrm{~d}_{2}$ | $\theta_{2}$ |
| 3 | 0 | 0 | $\mathrm{~d}_{3}$ | 0 |$\quad \mathbf{q}=\left[\theta_{1}, \theta_{2}, d_{3}\right]^{T}$

$$
\begin{gathered}
\mathbf{A}_{1}^{o}\left(\theta_{1}\right)=\left[\begin{array}{cccc}
c_{1} & 0 & -s_{1} & 0 \\
s_{1} & 0 & c_{1} & 0 \\
0 & -1 & 0 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \quad \mathbf{A}_{2}^{1}\left(\theta_{1}\right)=\left[\begin{array}{cccc}
c_{2} & 0 & s_{2} & 0 \\
s_{2} & 0 & -c_{2} & 0 \\
0 & 1 & 0 & d_{2} \\
0 & 0 & 0 & 1
\end{array}\right] \quad \mathbf{A}_{3}^{2}\left(d_{3}\right)=\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & d_{3} \\
0 & 0 & 0 & 1
\end{array}\right] \\
\mathbf{T}_{3}^{o}(\underline{q})=\mathbf{A}_{1}^{o} \cdot \mathbf{A}_{2}^{1} \cdot \mathbf{A}_{3}^{2}=\left[\begin{array}{cccc}
\mathrm{c}_{1} \mathrm{c}_{2} & -\mathrm{s}_{1} & \mathrm{c}_{1} \mathrm{~s}_{2} & \mathrm{c}_{1} \mathrm{~s}_{2} \mathrm{~d}_{3}-\mathrm{s}_{1} \mathrm{~d}_{2} \\
\mathrm{~s}_{1} \mathrm{c}_{2} & \mathrm{c}_{1} & \mathrm{~s}_{1} \mathrm{~s}_{2} & \mathrm{~s}_{1} \mathrm{~s}_{2} \mathrm{~d}_{3}+\mathrm{c}_{1} \mathrm{~d}_{2} \\
-\mathrm{s}_{2} & 0 & \mathrm{c}_{2} & \mathrm{c}_{2} \mathrm{~d}_{3} \\
0 & 0 & 0 & 1
\end{array}\right]
\end{gathered}
$$

## Spherical robot wrist

- Usually attached to the end of the robot arm

- All three axes of the rotational joints intersect in the same point

| Segment | $\mathrm{a}_{\mathrm{i}}$ | $\alpha_{\mathrm{i}}$ | $\mathrm{d}_{\mathrm{i}}$ | $\theta_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 4 | 0 | $-\pi / 2$ | 0 | $\theta_{4}$ |
| 5 | 0 | $\pi / 2$ | 0 | $\theta_{5}$ |
| 6 | 0 | 0 | $\mathrm{~d}_{6}$ | $\theta_{6}$ |

## Spherical robot wrist

| Segment | $\mathrm{a}_{\mathrm{i}}$ | $\alpha_{\mathrm{i}}$ | $\mathrm{d}_{\mathrm{i}}$ | $\theta_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 4 | 0 | $-\pi / 2$ | 0 | $\theta_{4}$ |
| 5 | 0 | $\pi / 2$ | 0 | $\theta_{5}$ |
| 6 | 0 | 0 | $\mathrm{~d}_{6}$ | $\theta_{6}$ |

$$
\mathbf{q}=\left[\theta_{4}, \theta_{5}, \theta_{6}\right]^{T}
$$

$$
\begin{aligned}
\mathbf{A}_{4}^{3}\left(\theta_{4}\right)=\left[\begin{array}{cccc}
c_{4} & 0 & -s_{4} & 0 \\
s_{4} & 0 & c_{4} & 0 \\
0 & -1 & 0 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \quad \mathbf{A}_{5}^{4}\left(\theta_{5}\right)=\left[\begin{array}{cccc}
c_{5} & 0 & s_{5} & 0 \\
s_{5} & 0 & -c_{5} & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \quad \mathbf{A}_{6}^{5}\left(\theta_{6}\right)=\left[\begin{array}{cccc}
c_{6} & -s_{6} & 0 & 0 \\
s_{6} & c_{6} & 0 & 0 \\
0 & 0 & 1 & d_{6} \\
0 & 0 & 0 & 1
\end{array}\right] \\
\mathbf{T}_{6}^{3}(\underline{q})=\mathbf{A}_{4}^{3} \cdot \mathbf{A}_{5}^{4} \cdot \mathbf{A}_{6}^{5}=\left[\begin{array}{cccc}
\mathrm{c}_{4} \mathrm{c}_{5} \mathrm{c}_{6}-\mathrm{s}_{4} \mathrm{~s}_{6} & -\mathrm{c}_{4} \mathrm{c}_{5} \mathrm{~s}_{6}-\mathrm{s}_{4} \mathrm{c}_{6} & \mathrm{c}_{4} \mathrm{~s}_{5} & \mathrm{c}_{4} \mathrm{~s}_{5} \mathrm{~d}_{6} \\
\mathrm{~s}_{4} \mathrm{c}_{5} \mathrm{c}_{6}+\mathrm{c}_{4} \mathrm{~s}_{6} & -\mathrm{s}_{4} \mathrm{c}_{5} \mathrm{~s}_{6}+\mathrm{c}_{4} \mathrm{c}_{6} & \mathrm{~s}_{4} \mathrm{~s}_{5} & \mathrm{~s}_{4} \mathrm{~s}_{5} \mathrm{~d}_{6} \\
-\mathrm{s}_{5} \mathrm{c}_{6} & \mathrm{~s}_{5} \mathrm{~s}_{6} & \mathrm{c}_{5} & \mathrm{c}_{5} \mathrm{~d}_{6} \\
0 & 0 & 0 & 1
\end{array}\right]
\end{aligned}
$$

## Stanford manipulator with the wrist



## Stanford manipulator with the wrist

$$
\begin{aligned}
& \mathbf{p}^{o}=\left[\begin{array}{c}
c_{1} s_{2} d_{3}-s_{1} d_{2}+\left(c_{1}\left(c_{2} c_{4} s_{5}+s_{2} c_{5}\right)-s_{1} s_{4} s_{5}\right) d_{6} \\
s_{1} s_{2} d_{3}+c_{1} d_{2}+\left(s_{1}\left(c_{2} c_{4} s_{5}+s_{2} c_{5}\right)+c_{1} s_{4} s_{5}\right) d_{6} \\
c_{2} d_{3}+\left(-s_{2} c_{4} s_{5}-c_{2} c_{5}\right) d_{6}
\end{array}\right] \\
& \mathbf{n}^{o}=\left[\begin{array}{c}
c_{1}\left(c_{2}\left(c_{4} c_{5} c_{6}-s_{4} s_{6}\right)-s_{2} s_{5} c_{6}\right)-s_{1}\left(s_{4} c_{5} c_{6}+c_{4} s_{6}\right) \\
s_{1}\left(c_{2}\left(c_{4} c_{5} c_{6}-s_{4} s_{6}\right)-s_{2} s_{5} c_{6}\right)+c_{1}\left(s_{4} c_{5} c_{6}+c_{4} s_{6}\right) \\
-s_{2}\left(c_{4} c_{5} c_{6}-s_{4} s_{6}\right)-c_{2} s_{5} s_{6}
\end{array}\right] \\
& \mathbf{s}^{o}=\left[\begin{array}{c}
c_{1}\left(-c_{2}\left(c_{4} c_{5} s_{6}+s_{4} c_{6}\right)+s_{2} s_{5} s_{6}\right)-s_{1}\left(-s_{4} c_{5} c_{6}+c_{4} c_{6}\right) \\
s_{1}\left(-c_{2}\left(c_{4} c_{5} s_{6}+s_{4} c_{6}\right)+s_{2} s_{5} s_{6}\right)+c_{1}\left(-s_{4} c_{5} c_{6}+c_{4} c_{6}\right) \\
s_{2}\left(c_{4} c_{5} s_{6}+s_{4} c_{6}\right)+c_{2} s_{5} s_{6}
\end{array}\right] \\
& \mathbf{a}^{o}=\left[\begin{array}{c}
c_{1}\left(c_{2} c_{4} s_{5}+s_{2} c_{5}\right)-s_{1} s_{4} s_{5} \\
s_{1}\left(c_{2} c_{4} s_{5}+s_{2} c_{5}\right)+c_{1} s_{4} s_{5} \\
-s_{2} c_{4} s_{5}+c_{2} c_{5}
\end{array}\right]
\end{aligned}
$$

## Inverse kinematics model

- Direct kinematics defines the pose of the end-effector depending on the internal coordinates
- Where will the end-effector move
- The pose of the end-effector is uniquely determined
$T(q)$
- Inverse kinematics defines the internal coordinates that would bring the robot endeffector in the desired pose
- How to move the end-effector to reach the desired pose
- Challenging problem:
- Nonlinear equations
- The solution is not uniquely defined
- Several solutions
- Sometimes even infinite number of solutions
- Sometimes the solution does not exist
- Take into account several criteria that determine which solution is optimal
- Sometimes we can get analytical solution, sometimes only numerical are possible


## ViCoS LCLWOS robot manipulator



## Requirements

## Low production cost

The cost of a single unit should be below $300 €$, it should use widely available components where possible.

Easy construction and maintenance
Construction from parts should be simpe, parts should be easily replaceable.

Simplicity and ease of use
The interaction with the platform should be multi-level

## Robustness

Both the hardware and software should be robust enough to withstand long-term use.

## Safety

The manipulator should be safe enough to be operated even by kids.

## Realism

The experience should be real enough for students of different university-level courses on robotics.

## Openness

Bot the hardware designs and software sources should be available for others to

## Related work



## Robot manipulator

Manipulator frame
All parts of manipulator frame
are created with a 3D printer
Joint motors
Move individual joints
and keep them positioned
Motor controllers
Low-level control of the
individual motors


## Forward model



## DH parameters:

| Segment | $a_{i}$ | $d_{i}$ | $\alpha_{i}$ | $\theta_{i}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0 mm | 48 mm | $90^{\circ}$ | $\theta_{1}$ |
| 2 | 108 mm | 0 mm | $0^{\circ}$ | $\theta_{2}$ |
| 3 | 112 mm | 0 mm | $0^{\circ}$ | $\theta_{3}$ |
| 4 | 0 mm | 0 mm | $90^{\circ}$ | $\theta_{4}$ |
| 5 | 0 mm | 90 mm | $0^{\circ}$ | $\theta_{5}$ |

## Transformation

$$
\begin{array}{rlrl}
A_{i}^{i-1}= & {\left[\begin{array}{cccc}
\cos \theta_{i} & -\sin \theta_{i} \cos \alpha_{i} & \sin \theta_{i} \sin \alpha_{i} & a_{i} \cos \theta_{i} \\
\sin \theta_{i} & \cos \theta_{i} \cos \alpha_{i} & -\cos \theta_{i} \sin \alpha_{i} & a_{i} \sin \theta_{i} \\
0 & \sin \alpha_{i} & \cos \alpha_{i} & d_{i} \\
0 & 0 & 0 & 1
\end{array}\right]} & A_{3}^{2}=\left[\begin{array}{cccc}
\cos \theta_{3} & -\sin \theta_{3} & 0 & a_{3} \cos \theta_{3} \\
\sin \theta_{3} & \cos \theta_{3} & 0 & a_{3} \sin \theta_{3} \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \\
A_{1}^{0}=\left[\begin{array}{cccc}
\cos \theta_{1} & 0 & \sin \theta_{1} & 0 \\
\sin \theta_{1} & 0 & -\cos \theta_{i} & 0 \\
0 & 1 & 0 & d_{1} \\
0 & 0 & 0 & 1
\end{array}\right] \\
A_{2}^{1}=\left[\begin{array}{cccc}
\cos \theta_{2} & -\sin \theta_{2} & 0 & a_{2} \cos \theta_{2} \\
\sin \theta_{2} & \cos \theta_{2} & 0 & a_{2} \sin \theta_{2} \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] & A_{4}^{3}=\left[\begin{array}{cccc}
\cos \theta_{4} & 0 & \sin \theta_{4} & 0 \\
\sin \theta_{4} & 0 & -\cos \theta_{4} & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \\
& A_{5}^{0}=A_{1}^{0} A_{2}^{1} A_{3}^{2} A_{4}^{3} A_{5}^{4}
\end{array}
$$

## Frame

- 3D printed


Frame parts


## Motors

- Servo motors


| Servo- <br> motor | Nape- <br> tost | Rotacijska <br> hitrost | Navor | Kratko- <br> stični <br> tok | Teža | Material <br> zobnikov |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| HS- | $4,8 \mathrm{~V}$ | $0,24 \mathrm{~s} / 60^{\circ}$ | $7,7 \mathrm{~kg} / \mathrm{cm}$ | $2,5 \mathrm{~A}$ | $55,2 \mathrm{~g}$ | kovina |
| 64.5 MG | $6,0 \mathrm{~V}$ | $0,20 \mathrm{~s} / 60^{\circ}$ | $9,6 \mathrm{~kg} / \mathrm{cm}$ |  |  |  |
| HS- | $4,8 \mathrm{~V}$ | $0,22 \mathrm{~s} / 60^{\circ}$ | $4,8 \mathrm{~kg} / \mathrm{cm}$ | $1,2 \mathrm{~A}$ | $45,0 \mathrm{~g}$ | karbonit |
| 48.5HB | $6,0 \mathrm{~V}$ | $0,20 \mathrm{~s} / 60^{\circ}$ | $6,0 \mathrm{~kg} / \mathrm{cm}$ |  |  |  |
| HS-311 | $4,8 \mathrm{~V}$ | $0,19 \mathrm{~s} / 60^{\circ}$ | $3,0 \mathrm{~kg} / \mathrm{cm}$ | $0,8 \mathrm{~A}$ | $43,0 \mathrm{~g}$ | najlon |
|  | $6,0 \mathrm{~V}$ | $0,15 \mathrm{~s} / 60^{\circ}$ | $3,5 \mathrm{~kg} / \mathrm{cm}$ |  |  |  |
| ES08AII | $4,8 \mathrm{~V}$ | $0,12 \mathrm{~s} / 60^{\circ}$ | $1,5 \mathrm{~kg} / \mathrm{cm}$ | $0,7 \mathrm{~A}$ | $8,5 \mathrm{~g}$ | najlon |
|  | $6,0 \mathrm{~V}$ | $0,10 \mathrm{~s} / 60^{\circ}$ | $1,8 \mathrm{~kg} / \mathrm{cm}$ |  |  |  |

## Upgrading servomotors

- New control circuit
- Potentiometer
- OpenServo
- Current protection



## PID controller

## - Proportional, integral and derivative part

$$
u\left(t_{k}\right)=K_{p} e\left(t_{k}\right)+K_{i} \sum_{n=1}^{k} e\left(t_{n}\right) \Delta t+\frac{e\left(t_{k}\right)-e\left(t_{k-1}\right)}{\Delta t}
$$

1: // Proporcialni del
2: p_component $=$ seek_position - current_position;
3: pwm_output $=\left(\right.$ int $32 \_$_t $) p_{-}$component $*\left(\right.$ int $\left.32_{-} t\right) p_{-}$gain $;$
4: // Odvodni del
5: d_component $=(\text { p_component }- \text { p_component_old })^{\text {com }} 256$;
6: pwm_output+ $=\left(\right.$ int $\left.32 \_t\right) d \_c o m p o n e n t ~ *\left(\right.$ int $\left.32 \_t\right) d \_g a i n$;
7: // Integralni del
8: i_component+ = p_component;
9: pwm_output $+=\left(\left(\left(\right.\right.\right.$ int $\left.32 \_t\right) i_{\_}$component $*\left(\right.$ int $\left.32 \_t\right) i_{-}$gain $\left.) \gg 8\right)$;

| Sklep | $K_{p}$ | $K_{i}$ | $K_{d}$ |
| :---: | :---: | :---: | :---: |
| S1 | 500 | 300 | 5 |
| S 2 | 500 | 300 | 5 |
| S 3 | 500 | 300 | 5 |
| S 4 | 300 | 200 | 5 |
| S 5 | 150 | 200 | 5 |
| Prijemalo | 500 | 200 | 5 |

10: //
11: pwm $=\left(\left(\right.\right.$ int $\left.16 \_t\right)($ pwm_output $\left.\gg 8)\right)$;

## AD converter

- Increasing resolution
- Multiple sampling and decimation
- Resolution increased from 10 to 12 bits
- Sampling frequency 256 Hz

$$
A D C_{(10+n) b i t}=\frac{\sum_{k=1}^{4^{n}} A D C_{10 b i t}}{2^{n}}
$$

| Ločljivost | Čas branja | Največja frekvenca |
| :---: | :---: | :---: |
| 10 bitov | $\approx 0,0864 \mathrm{~ms}$ | $\approx 11574 \mathrm{~Hz}$ |
| 11 bitov | $\approx 0,3456 \mathrm{~ms}$ | $\approx 2893 \mathrm{~Hz}$ |
| 12 bitov | $\approx 1,3824 \mathrm{~ms}$ | $\approx 723 \mathrm{~Hz}$ |
| 13 bitov | $\approx 5,5296 \mathrm{~ms}$ | $\approx 180 \mathrm{~Hz}$ |

## Communication

- $\mathrm{I}^{2} \mathrm{C}$ interface
- $I^{2} \mathrm{C}$ bus
- OpenServo
- Communication with microcontroller
- OpenServoRobot
- Robot model (DH parameters)
- Communication with application



## Workspace



## Theoretical accuracy

- Expected deviation of the estimated position from the reference position of the end effector
- Only considering motor errors
- Theoretical upper limit of precision

| Osi | Odstopanje (mm) |  |  | Standardni odklon (mm) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Najmanj | Največ | Povprečno | Najmanj | Največ | Povprečno |
| x | 0,00 | 0,45 | 0,14 | 0,01 | 0,61 | 0,20 |
| y | 0,00 | 0,45 | 0,14 | 0,00 | 0,61 | 0,21 |
| z | 0,00 | 0,44 | 0,16 | 0,03 | 0,56 | 0,66 |
| d | 0,10 | 0,55 | 0,29 | 0,14 | 0,73 | 0,41 |

## Theoretical accuracy



## Theoretical accuracy



## Empiciral repetabilty



| Meritev | Os x | Os y |
| :---: | :---: | :---: |
| Blizu | $1,4 \mathrm{~mm}$ | $0,6 \mathrm{~mm}$ |
| Daleč | $3,8 \mathrm{~mm}$ | $0,7 \mathrm{~mm}$ |




## Calibration



## Characteristics



| Lastnost | Vrednost |
| :---: | :---: |
| Višina | 358 mm |
| Radij | 310 mm |
| Ponovljivost | 4 mm |
| Teža | 842 g |
| Nosilnost | 80 g |
| Napajanje | $5,0 \mathrm{~V}$ |
| Tok | 6000 mA |

## Integration in ROS



## Integration in Manus



## Integration with programming languages

- Matlab
- Python
- Blockly



## Communication using VGA and USB cable

- VGA cable and $I^{2} \mathrm{C}$ protocol
- USB port



## Registration with camera



## Augmented reality

Camera view
USB Robot Manipulator (version: 0.10)



## Multi-level teaching approach



Simulated
Environment and manipulator are both simulated.


## Augmented

Simulated manipulator is superimposed on real world.


Real-world
Real manipulator is used in real world.

| perception | action | activity |  |
| :---: | :---: | :---: | :--- |
| 1 simulated | none | Learning basic computer vision algorithms by processing <br> stored images. |  |
| 2 | real | none | Learning more advanced computer vision algorithms by <br> capturing and processing live images. |
| 3 | none | simulatedLearning the basics of robot manipulation in simulated <br> environment. |  |
| 4 | none | real | Learning to operate the robot manipulator in the real <br> world. |
| 5 | real | simulated |  | with the virtual robot manipulator.

6 real real Detecting and grasping the objects in the scene with the physical robot manipulator.

## Video



## Mobile manipulation



## Vision-based control



- Camera on the robot
- Fixed camera

Moving the end effector to the desired pose determined by the pose of an object


## Vision-based control

- Position-based servoing
- Explicit control
- In world coordinate frame

- Image-based servoing
- Implicit control
- In image coordinate frame



## Vision-based control



## Vision-based control

- Mobile manipulation
- Joint control of mobile robot and robot manipulator


